

1 The efficiency of sieve-panels for bycatch separation in *Nephrops* trawls

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18

19 **Abstract**

20 This study investigates the efficiency of a sieve-panel concept, intended to separate bycatch

21 species from *Nephrops* (Norway lobster) in a trawl gear via mechanical and behavioral means.  
22 Four different designs of varying panel mesh size or inclination were tested in experimental  
23 fishing. For each design, we estimated the length-dependent sieving efficiency, defined as the  
24 fraction of *Nephrops* or fish passing through the panel to the lower codend. The sieving  
25 efficiency for *Nephrops* increased from ~17% to ~71% as mesh size increased, and it decreased  
26 with increasing carapace length, but did so less as panel inclination and mesh size increased. The  
27 sieving efficiency for roundfish was low, as intended, while the efficiency for flatfish decreased  
28 with fish size. Although results are promising, the sieving efficiency for the largest, most  
29 valuable *Nephrops* remained too low. Therefore, further improvements are necessary before the  
30 concept is acceptable to the commercial fishing fleet.

31 Keywords: *Nephrops*, bycatch, trawl, sieve-panel, efficiency, Landing Obligation

## 32 **1. Introduction**

33 *Nephrops* (*Nephrops norvegicus*) directed fisheries are among the economically most important  
34 fisheries in European waters (Ungfors et al., 2013). Although some creel fisheries target  
35 *Nephrops* (Adey, 2007), 95% of total European landings are taken by demersal trawlers (Briggs,  
36 2010; Ungfors et al., 2013). Catching *Nephrops* efficiently with trawls requires using relatively  
37 small mesh codends (Krag et al., 2008; Frandsen et al., 2010), which can lead to large bycatches  
38 of small fish co-habiting the fishing grounds (Alverson et al., 1994; Catchpole and Revill, 2008;  
39 Catchpole et al., 2007; Kelleher, 2005; Krag et al., 2008).

40 The problem of unwanted bycatch in *Nephrops* fisheries has been addressed mainly by  
41 attempting to provide additional escapement possibilities for fish species before they enter the  
42 codend (Catchpole and Revill, 2008). Although different in concept and purpose, all current

43 devices are designed to reduce bycatch by selecting fish out of the catch. Probably the most used  
44 bycatch reduction devices (BRDs) are the Swedish grid (Valentinsson and Ulmestrand, 2008) for  
45 monospecific *Nephrops* fisheries, and square mesh panels (SMPs) for mixed fisheries  
46 (Armstrong et al., 1998; Briggs, 1992). Although it has been demonstrated that using these BRDs  
47 can significantly reduce bycatch rates, to date none of them have delivered an efficient size  
48 selectivity for the target and bycatch species simultaneously. Depending on the population  
49 structure fished, this can lead to a considerable number of bycaught small fish (Frandsen et al.,  
50 2009; Lövgren et al., 2016; Nikolic et al., 2015; Valentinsson and Ulmestrand, 2008), or losses of  
51 marketable *Nephrops* (Catchpole et al., 2006; Frandsen et al., 2009).

52 Achieving an efficient size selection for both the target and bycatch species is an increasingly  
53 important requirement in the wake of the Common Fisheries Policy (CFP) reform (EU 2013),  
54 implemented in *Nephrops* fisheries since 2016. The reform adopted the Landing Obligation (LO)  
55 for listed species, which forces fishers to land all catches of those species and count them against  
56 their quota. Under such a scenario, a large bycatch of fish species with limited quota can alter the  
57 fishing strategy or even force fishers to stop fishing completely, without exhausting the quota of  
58 *Nephrops*. Improving species and size selectivity is required now more than ever to secure both  
59 the biological and economical sustainability of *Nephrops*-directed fisheries.

60 This study presents an alternative concept for reducing fish bycatch in these fisheries. Our  
61 concept shares similarities with the sieve nets used in shrimp trawl fisheries, such as the brown  
62 shrimp fishery in the North Sea (Revill and Holst; 2004), and it is based on the assumptions that  
63 *Nephrops* has limited swimming activity and tends to roll over the floor of the trawl body  
64 (Briggs and Robertson, 1993; Main and Sangster, 1985), whereas fish tend to swim actively to

65 stay clear of the surrounding net (Glass and Wardle, 1995). It consists of a 10-m-long square  
66 mesh sieve-panel, mounted in the extension piece of the trawl with a continuous upward  
67 inclination towards an upper and lower codend. The fore edge of the sieve-panel is attached to  
68 the floor of the gear, ensuring that all *Nephrops* and fish will enter on the upper side of the panel  
69 connected to the upper codend. Assuming that the behavioral differences between *Nephrops* and  
70 the fish species listed above can be utilized, the panel will sieve *Nephrops* towards the lower  
71 codend, and fish will be guided towards the upper codend. The mesh size used in the sieve- panel  
72 and its inclination should be sufficiently large to sieve all sizes of *Nephrops* towards the lower  
73 codend, without losing the ability to guide fish to the upper codend.

74

75 The aim of the study is to investigate and quantify the ability of different sieve-panel designs to  
76 separate *Nephrops* from different roundfish and flatfish species during the catching process.

## 77 **2. Material and Methods**

### 78 *2.1 Sieve-panel designs and test gear*

79 The 10-m-long sieve-panel was mounted in the four-panel extension piece of the trawl (Figure  
80 1). The fore edge of the sieve-panel was attached at the front of the extension's lower panel, and  
81 the sides were connected to the lateral panels with a cutting rate of 6N2B. This construction  
82 provides a monotonous upward–backward inclination of  $\sim 2.5^\circ$ , and splits the aft of the trawl into  
83 two horizontal compartments, ending in the lower and upper codend (Figure 1).

84 Four different panel designs were tested during experimental fishing. All designs used square  
85 mesh netting (Figure 1). Design 1 was made of knotless PA netting with 45.2 mm measured bar

86 length and 2.5 mm nominal twine thickness. Design 2 used knotless PE netting with 60.9 mm bar  
87 length and 5 mm twine thickness. Design 4 was constructed similarly to Designs 1 and 2, but  
88 used PE standard netting, with 94.3 mm mesh bar length and 3 mm twine thickness. Design 3  
89 used the same sieve-panel as Design 2, but the monotonous inclination was altered by inserting  
90 six floating lines, arranged in two groups of three and attached at two different positions on the  
91 panel's lower side. The configuration was intended to create a hilly surface to increase the  
92 inclination of the panel (Figure 1). For a sieve-panel to perform well, sieving efficiency should  
93 be high for all sizes of *Nephrops* and low for all sizes of the bycatch species.

94 During experimental fishing, the sieve-panels were mounted one at a time for a group of hauls in  
95 the same extension piece, which was 11.5 m long, made of PE single netting with 1.8 mm twine  
96 thickness. The stretched mesh size obtained with the omega gauge (Fonteyne et al., 2007) was  
97 47.9 mm (Figure 1). The codends were 6 m long and made of PA netting with ~1.2 mm twine  
98 thickness. The stretched mesh sizes of the codends were 48.4 mm and 49.6 mm for the upper and  
99 lower codends, respectively. The codend mesh sizes applied were considered sufficiently small to  
100 retain all *Nephrops* available in the targeted population. The extension piece and the double  
101 codend system were connected to a demersal trawl model Spaeghugger, spread by two Thyborön  
102 doors Type 2 (1.78 m<sup>2</sup>).

### 103 *2.3 Sea trials and data collection*

104 The four sieve-panels were tested September 12–24, 2015, on Danish *Nephrops* fishing grounds  
105 in the Skagerrak (ICES Division IIIa), using the German research vessel “Solea” (42 m, 1780  
106 kW). Catches obtained at haul level were sampled by species and for each codend separately.

107 Catch weight was collected using electronic scales. The *Nephrops* carapace length (CL) was  
108 measured to the nearest 0.5 mm using digital calipers. Total length (TL) was measured to nearest  
109 0.5 cm for the fish bycatch species using electronic measuring boards. Subsampling was avoided  
110 in most of the experimental hauls. When subsampling occurred, the subsampling factor was  
111 calculated by dividing the subsampling weight by the total catch weight.

112 Underwater video recordings were collected during the experimental hauls to qualitatively assess  
113 the shape of the sieve panel and how different species interacted with it. The cameras used were  
114 GoPro model Hero 3+, mounted in deep-water housing, model GoBenthic2. The camera system  
115 was supplemented with flood-beam artificial light (1400 lumens).

116

#### 117 2.4 Data analysis

118 The sieving efficiency was quantified separately for each of the sieve-panels and each species as  
119 described below.

120 With  $nlc_{il}$  as the number of individuals of length  $l$  (CL or TL) caught in the lower codend during  
121 Haul  $i$ , and  $nuc_{il}$  as the number of length  $l$  caught in the upper codend, the proportion of the total  
122 catch observed in the lower codend,

$$123 \quad S_{il} = \frac{nlc_{il}}{nlc_{il} + nuc_{il}}, \quad (1)$$

124 can be interpreted as the experimental sieving efficiency of the sieve-panel for individuals with  
125 length  $l$ .  $S_{il}$  can only take values in the range 0.0–1.0. Values of  $S_{il}$  close to 1.0 would mean that

126 most individuals with length  $l$  were sieved and finally retained in the lower codend. On the other  
 127 hand,  $S_{il}$  values close to 0.0 would mean low sieving efficiency, either because individuals of  
 128 length class  $l$  were not physically able to pass through the meshes, or because the sieve-panel  
 129 guided them towards the upper codend.

130 The sieving efficiency might be influenced by the size selection of the square meshes and by  
 131 species behavior when interacting with the sieve-panel, which at the same time might be length  
 132 dependent. Therefore, length-dependent sieving efficiency is modelled by applying a highly  
 133 flexible function  $S(l, \mathbf{q})$ :

134

$$135 \quad S(l, \mathbf{q}) = \frac{\exp(f(l, q_0, \dots, q_j))}{1 + \exp(f(l, q_0, \dots, q_j))}, \quad (2)$$

136 where  $f$  is a polynomial of order  $j$ , with coefficients  $q_0$  to  $q_j$ , which provide great flexibility to the  
 137 functional form of the resulting sieve efficiency curve. The estimation of the values of the  
 138 parameters  $\mathbf{q} = (q_0, \dots, q_j)$ , which make the observed experimental data averaged over hauls most  
 139 likely, was carried out by minimizing the negative log likelihood function for the binomial data:

$$140 \quad \log L_{model} = - \sum_i \sum_l \{n_{lc_{il}} \times \ln(S(l, \mathbf{q})) + n_{uc_{il}} \times \ln(1.0 - S(l, \mathbf{q}))\}, \quad (3)$$

141 where the summations are for group of hauls  $i$  with the specific sieve-panel design and length  
 142 classes  $l$ . In Equation 2, we considered  $f$  as a polynomial up to the order 4 with parameters  $q_0, q_1,$   
 143  $q_2, q_3,$  and  $q_4$ . Leaving out one or more of the parameters  $q_0$ – $q_4$  led to 31 additional simpler  
 144 models that were also considered potential candidates for the sieve efficiency curves  $S(l, \mathbf{q})$ , and

145 therefore they were also estimated using Equation 3. Selection of the best model for  $S(l, q)$  among  
146 the 32 competing models was based on a comparison of their respective Akaike information  
147 criterion (AIC) values (Akaike, 1974). The model with the lowest AIC value was selected to  
148 describe the experimental sieving efficiency.

149 The model's ability to describe the data was evaluated based on an inspection of the fit statistics,  
150 i.e. the  $p$ -value and the model deviance vs. the degrees of freedom (df), following the procedures  
151 described by Wileman et al. (1996). The  $p$ -value expresses the likelihood of obtaining a  
152 discrepancy at least as large as between the fitted model and the observed experimental data by  
153 coincidence. In case of poor fit statistics ( $p$ -value  $< 0.05$ ; deviance  $\gg$ df), we examined if the  
154 poor result was caused by structural problems when describing the experimental data using the  
155 model, or if it was the result of overdispersion in the data (Wileman et al., 1996).

156 The 95% confidence intervals (CI) for the averaged sieve efficiency curve  $S(l, q)$  were estimated  
157 using a double bootstrap method with 1000 replications. This approach, which avoided  
158 underestimating confidence limits when averaging over hauls, is identical with the one described  
159 in Sistiaga et al. (2010). Traditionally, the CIs are estimated without accounting for potentially  
160 increased uncertainty resulting from uncertainty in the selection of the model used to describe the  
161 curve (Katsanevakis, 2006). Following the same method used by Krag et al. (2015), we  
162 accounted for this additional uncertainty, by incorporating an automatic model selection based on  
163 which of the 32 models produced the lowest AIC for each of the bootstrap iterations.

164 In addition to the assessment of the uncertainty of the individual averaged sieve curves, the  
165 bootstrap CIs were used to compare *Nephrops* sieving efficiencies obtained for the different  
166 sieve-panel designs. Such assessments were carried out as pairwise comparisons, and the



167 differences within pairs were considered statistically significant only in the range of individual  
168 lengths, where the compared CIs did not overlap. The analysis of sieve-panel efficiency was  
169 carried out using the software tool SELNET (Herrmann et al., 2012).

170

### 171 **3. Results**

#### 172 *3.1. Description of experimental hauls and catches*

173 The experimental hauls were conducted in Danish fishing grounds within 57°–58°N and 009–  
174 010°E (Figure S1 in supporting material) at fishing depths between 54 and 136 m (Table 1). Haul  
175 duration ranged from 28 to 118 minutes. In all, 13, 10, 7, and 11 valid hauls were conducted  
176 using Designs 1, 2, 3, and 4, respectively, a total of 41 experimental hauls. A total of 108  
177 *Nephrops* were caught and measured with Design 1, a very small number compared with the  
178 2155, 3669, and 1627 individuals measured in Designs 2–4 (Table 1). Two roundfish and two  
179 flatfish species were caught in sufficient numbers to warrant investigating the sieving  
180 efficiencies on the fish species: American plaice (*Hippoglossoides platessoides*, 45363 fish  
181 measured), blue whiting (*Micromesistius poutassou*, 13677 fish measured), cod (*Gadus morhua*,  
182 7804 fish measured), and witch flounder (*Glyptocephalus cynoglossus*, 5471 fish measured;  
183 Table 1).

184 Of the *Nephrops* caught in the hauls with Design 1, 17% were collected in the lower codend,  
185 increasing to 71% with Design 4 (Table 1). On the contrary, less than 10% of the cod, blue  
186 whiting, and witch flounder caught were observed in the lower codend. Larger numbers of  
187 American plaice were observed in the lower codend than the other fish species, increasing from

188 12% with Design 1 to 50% with Design 4.

189 A short haul in shallow and clear waters was conducted to collect video recordings showing the  
190 shape and mechanical behavior of the extension piece with the sieve-panel mounted. video  
191 recordings were collected during seven of the experimental hauls (Table 1), for a total of 561  
192 minutes. Exploratory analysis of catch data indicated no clear influence of the camera system on  
193 sieve panel performance; therefore, these hauls were used in the quantitative analysis.

### 194 3.2. Assessment of the length-dependent sieving efficiency

195 The sieving efficiency of each of the sieve-panel designs was successfully obtained using the  
196 model described in Equation 2.  $P$ -values  $>0.05$  were obtained in all cases, except for *Nephrops* in  
197 Design 4, confirming the model's ability to describe the length-dependent sieving efficiency in  
198 the experimental data (Table 2). The low  $p$ -value obtained for *Nephrops* Design 4 could indicate  
199 the model's inability to describe the experimental data. However, inspection of the deviations  
200 between the observed and modelled sieving efficiency did not reveal any clear pattern (Figure 2).  
201 Therefore, we concluded that, in this case, the low  $p$ -value was caused by overdispersion in the  
202 experimental data; therefore, we were confident in applying the model to describe the sieving  
203 efficiency curve for *Nephrops* in Design 4 as well.

204 The model for *Nephrops* predicted a sieving curve with values of less than 40% for Design 1,  
205 decreasing in efficiency as carapace length increased (Figure 2). Larger percentages of *Nephrops*  
206 catches were sieved using Designs 2–4, but many of the large individuals were still found in the  
207 upper codend. The larger mesh size applied in Design 2 improved the sieving efficiency of  
208 Design 1 significantly, estimated as being greater than 86% for  $CL \leq 30$  mm, but decreasing

209 drastically as CL increased. Increasing the inclination with the float lines applied in Design 3  
210 reduced the monotonic decreasing trend in the sieving efficiency curve from Design 2, thereby  
211 reducing the loss in sieving efficiency for the largest sizes. Finally, Design 4 clearly reduced the  
212 negative trend observed in the previous designs, and the average sieving efficiency was not lower  
213 than 45% throughout the experimental CL classes (Figure 2).

214 The increased mesh sizes from Design 1 to Design 2 resulted in an overall and significant  
215 improvement in sieving efficiency, except for CL, which was larger than ~60 mm. Design 3's  
216 sieving values were higher on average than Design 2's, but the improvement was not statistically  
217 significant over the available CL range. Design 4 improved the sieving efficiency of Designs 2  
218 and 3 on CL ~50 mm significantly and the efficiency of Design 2 on CL greater than 60 mm  
219 (Figure 2).

220 For the bycatch species, less than 1% of cod (18 fish) were caught in the lower codend using  
221 Design 1. A larger number of individuals (4.3%) were sieved in Design 2, mostly in the range of  
222 20–40 cm TL. Designs 3 and 4 increased the probability of small cod being sieved towards the  
223 lower codend. Nevertheless, the averaged sieve curve from Design 4 remains below 20% for  
224 most of the TL classes available (Figure 3).

225 Negligible catches (3%) of blue whiting were observed in the lower codend over the different  
226 designs. Only the steeper inclination of the panel in Design 3 resulted in an increased sieving  
227 efficiency for TL less than 30 cm, however still less than 20% (Figure 3).

228 A considerable number of American plaice were observed in the lower codend and, as with  
229 *Nephrops*, the sieving efficiency was strongly and negatively related to fish length. Similar

230 curves were obtained for Designs 1–3. Sieving efficiency was increased over the whole length  
231 range by Design 4 (Figure 4).

232 Sieve efficiency was lower and less dependent on fish length for witch flounder than for  
233 American plaice. Consistent with results from the previous flatfish species, Design 4 raised the  
234 sieving efficiency obtained by the other three designs considerably (Figure 4).

235

### 236 3.3. Underwater video recordings

237 The images collected confirmed that the shape of the sieve-panels were as intended. The sieve-  
238 panel had a slight U-shape resulting from the drag of the water flow during towing (Figure S2 in  
239 supporting material).

240 The sediments suspended in the water column made it difficult to collect quality video  
241 sequences, and only a few of them revealed *Nephrops* interacting with the sieve-panels. Contrary  
242 to expectations, most observations of *Nephrops* passing through the sieve-panel meshes occurred  
243 through individuals' active behavior. One observation involved a first swimming phase, where  
244 the individual contacted an open mesh tail-first (Figure S3, A.1 in supporting material). After  
245 penetrating the mesh tail-first, the individual pushed the body downwards attempting to burrow  
246 below the sieve-panel (Figure S3, A.2 in supporting material). At this stage, the individual stayed  
247 with the claws upwards above the panel surface, and most of the body below it (Figure S3, A.3 in  
248 supporting material), before pushing downwards again to pass the mesh completely and fall into  
249 the lower compartment (Figure S3, A.4 in supporting material). On the contrary, other  
250 individuals actively avoided being sieved by lying on the bar meshes (Figure S3, B in supporting

251 material), holding the mesh twines with the chelipeds, both in the natural or reverse body  
252 orientation (Figure S3, C-E in supporting material), or simply by walking over the panel. In the  
253 last case, some specimens were observed walking over the panel until they lost their balance and  
254 finally drifted with the water flow towards the upper codend.

255 Most fish observed in the recordings followed the bottom–up inclination of the sieve-panel  
256 without attempting to pass through the meshes. Few active passages of cod were observed during  
257 the haul-back process, when cod attempted to swim downwards to balance the decrease in  
258 hydrostatic pressure caused by the loss of depth.

259

#### 260 **4. Discussion**

261 The progressive improvement in *Nephrops* sieving efficiency from Design 1 to Design 4 was  
262 related to increments in the mesh size applied to the different panels. Although Design 2 clearly  
263 improved on the performance of Design 1, the strong and negative length dependence in the  
264 efficiency of this design makes it unfeasible for commercial adoption. Further increasing the  
265 mesh size in Design 4 reduced the length dependence of the average sieve curve, but even with  
266 such improvement, only 45% of the *Nephrops* larger than 55 mm CL were found in the lower  
267 codend. Although Design 3 did not improve significantly on the efficiency of Design 2, the form  
268 of the predicted curve indicates that increasing the inclination of the panel might benefit the  
269 sieving efficiency..

270 Contrary to the original design assumptions, many sieving events observed in the underwater  
271 video recordings occurred when individuals actively positioned the body in an optimal

272 orientation towards the open meshes (Figure S3, A1–A4 in supporting material), whereas other  
273 active interactions counteracted the sieving process (Figure S3, B–E in supporting material).  
274 Based on the quantitative results and observation of the video recordings, we speculate that, in  
275 addition to the passive process assumed in the design of the device, the sieving of *Nephrops*  
276 might also be influenced by avoidance behavior, which could be stronger in large individuals.  
277 Investigations conducted in tank aquariums demonstrated length-dependent avoidance behavior  
278 only for male *Nephrops* (Newland et al., 1998). In particular, it was observed that larger males  
279 reacted to tactile stimulus by producing fewer swimming bouts with more tail-flips per bout than  
280 smaller individuals. Assuming that these findings can be extrapolated to the fishing grounds, we  
281 speculate that avoidance behavior expected for large individuals could reduce the number of  
282 times they contact the surface of the sieve panel compared to smaller individuals, reducing  
283 therefore the sieving occurrences. Since the relationship between swimming performance and  
284 individual length was found sex-dependent, *Nephrops* sex ratios in both the lower and upper  
285 codend could be used as indicators to clarify if the behavioral observations in Newland *et al.*  
286 (1998) could explain the length-dependent efficiency of the gear.

287 The sieving efficiency of cod was estimated at less than 20% for all reference lengths considered  
288 (Table 3). In particular, the efficiency of TL = 34 cm was 13%, meaning that 87% were directed  
289 towards the upper codend. It was assumed that using *Nephrops*-selective netting in the lower  
290 codend would provide some escapement possibilities for small fish, thus lowering even further  
291 the catch probability of undersized cod. The combination of a sieve-panel and selective codends  
292 would therefore significantly improve the cod bycatch rates in trawls mounting the Swedish grid,  
293 estimated at ~30% for lengths ~34 cm (Lövgren et al., 2016).

294 The sieve-panel performed differently on roundfish and flatfish. The greater and strongly length-  
295 dependent sieving efficiency observed for flatfish species is a consequence of their natural  
296 behavior, tending to swim in close contact with the floor of the net (Ryer, 2008), and therefore  
297 increasing the probability of being mechanically sieved to the lower codend.

298 Although the sieve-panel concept tested here is a promising tool for improving the exploitation  
299 patterns in *Nephrops* fisheries, further improvements are necessary before the concept will be  
300 acceptable to commercial fishing fleets. The results of the present study provide further  
301 development opportunities of the concept in three different dimensions. First, a steeper  
302 inclination of the sieve-panel could improve the sieving efficiency for *Nephrops*. We speculate  
303 that this alteration in the original design might reduce the longitudinal transportation of  
304 *Nephrops* over the panel, enhancing the possibility of being sieved through the meshes. On the  
305 downside, a steeper angle might reduce the guiding effect, leading to larger fractions of fish  
306 passing through the panel into the lower codend. Alternative mounting angles to be considered  
307 for future designs should be between 30° and 45°, a range used for other devices applied in  
308 *Nephrops* fisheries such as the Swedish grid (Valentinsson and Ulmestrand, 2008), or separator  
309 panels (Rihan and McDonnell, 2003). Increasing the mesh size used in Design 4 could facilitate  
310 the sieving efficiency for *Nephrops*, whereas changing the mesh geometry to a rectangular shape  
311 with the longitudinal opening oriented in the towing direction might reduce the sieving efficiency  
312 for flatfish, because of the species' flat body shape. Finally, using thicker twine in the panel  
313 construction might limit the *Nephrops*' ability to hold the twines and avoid being sieved.

314 Efficient separation of *Nephrops* and fish species might substantially reduce the unwanted  
315 bycatch in European *Nephrops*-directed fisheries. By securing the *Nephrops* catch in a lower

316 codend, fishers could mount an upper codend with a larger mesh size to catch larger fish. Under  
317 fish quota exhaustion, catches of fish might be avoided by opening the upper codend during  
318 towing. In addition to a better utilization of available quotas, other benefits can be expected by  
319 dividing the species efficiently into separate codends: A proper separation would improve the  
320 quality of marketable fish catches, as they are not subjected to damages in the skin and internal  
321 tissues caused by the contact with the spiny appendixes of *Nephrops* (Karlsen et al., 2015;  
322 Galbraith and Main, 1989). Exemptions to the Landing Obligation are contemplated in the  
323 European legislation for species with scientific evidences of high survival rates after catch and  
324 release. Most recent studies on *Nephrops* reported survival rates in the range of ~20-60%  
325 (Méhault et al., 2016; Castro et al., 2003), therefore *Nephrops* could be one of these exemptions  
326 under evidences of improved survival rates. Achieving “clean” *Nephrops* catches would  
327 drastically reduce the overall catch volume in the lower codend, sorting time on deck and air  
328 exposure, improving survival probability (Méhault et al., 2016; Harris and Andrews, 2005;  
329 Castro et al., 2003).

330 Further investigations combining quantitative analysis of *Nephrops* behavioral patterns with  
331 sieve-panels having different inclinations, mesh geometries, and twine thickness are planned.  
332 Such future investigations could provide a better understanding of how mechanical and  
333 behavioral size selection contributes to the observed sieving efficiency for *Nephrops*. This  
334 information is required to create design guides for more efficient *Nephrops* sieve-panels to  
335 achieve clean *Nephrops* catches in the lower codend, while ensuring minimal or no losses of  
336 marketable individuals, so providing the industry with new technological alternatives to dealing  
337 with the landing obligation enforced by the new European Fishing Policy.



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466

467 Table 1. Summary of hauls conducted with the different *Nephrops* sieve-panel designs, including  
 468 the average towing duration (standard deviation in round brackets), and the number of individual  
 469 length-measurements obtained from each of the analyzed species and sampling compartments.  
 470 Subsampling rates are presented in square brackets for those cases where not all fish were  
 471 measured.  
 472

Design	Number hauls	Duration (minutes)	<i>Nephrops</i>		Cod		Blue whiting		American plaice		Witch flounder	
			Lower codend	Upper codend	Lower codend	Upper codend	Lower codend	Upper codend	Lower codend	Upper codend	Lower codend	Upper codend
1	13	54.5 (31.0)	19	89	18	2082	33	2530	1609	6246 [0.973]	0	1085
2	10	100 (29.0)	1349	806	76	1693	24	3863 [0.700]	2561	6799 [0.885]	12	1034
3	7	100.9 (16.0)	2537	1132	31	563 [0.998]	376	3606	2570	7110	14	898
4	11	96.4 (13.9)	1156	471	106	1135	18	664 [0.730]	5393	5220 [0.856]	134	1209 [0.799]



473 Table 2. Sieving efficiency model statistics for the different species analyzed (df = model degrees of  
 474 freedom, n hauls = number of hauls included in the analysis).

Species	Parameter	Design 1	Design 2	Design 3	Design 4
<i>Nephrops</i>	P-value	0.90	0.86	0.15	0.04
	deviance	36.79	72.07	98.68	101.29
	df	49	86	85	78
	n hauls	2	10	7	7
<i>Cod</i>	P-value	>0.99	>0.99	>0.99	0.99
	deviance	56.90	50.54	34.57	64.78
	df	111	108	86	93
	n hauls	13	10	7	11
<i>Blue whiting</i>	P-value	0.87	0.99	0.98	0.98
	deviance	41.62	30.8	29.96	23.35
	df	53	51	48	39
	n hauls	7	9	7	11
<i>American plaice</i>	P-value	0.13	>0.99	0.97	0.65
	deviance	54.76	25.14	30.48	42.81
	df	44	50	47	47
	n hauls	7	10	7	11
<i>Witch flounder</i>	P-Value	>0.99	>0.99	0.95	0.64
	deviance	0.00	23.52	35.41	46.89
	d.o.f	47	51	51	51
	n hauls	11	10	7	11

475 **Figure captions:**

476

477 Figure 1. Top: Side view of the experimental gear with the general design of the sieve-panel  
478 (blue stippled line) mounted ahead of the double codend setup. For the sorting system to work  
479 efficiently, the following selection events have to take place consistently: (1) Assuming that  
480 *Nephrops* travels towards the codends by rolling and hitting the lower panel of the net, it is  
481 expected that they will be sorted by the sieve-panel to the lower codend (orange path); (2) the  
482 bottom–up inclination of the panel should guide fish upwards towards the upper codend (green  
483 path). Middle: Number of meshes of the different sieve-panel designs; additional floats (blue)  
484 were mounted in Design 3. Bottom: Netting used in the different designs and the measured mesh  
485 bar length of each (s.d. in parentheses). Nets were scanned using the same scale, allowing a  
486 direct comparison between meshes.

487

488 Figure 2. First and second rows show the sieving efficiency curves (solid lines), 95% bootstrap  
489 CIs (dashed lines), and experimental sieving data (points) obtained for *Nephrops* by each sieve-  
490 panel design (D1= Design 1 ,..., D4= Design 4). Total catches (light grey shading) and catches in  
491 lower codend (dark grey shading) are plotted in the background. Third and fourth rows show  
492 pairwise comparisons of the *Nephrops* sieving efficiency achieved by each of the designs. The  
493 grey bands represent the CI associated to each of the estimated sieving efficiency curves. The  
494 top-right to bottom-left diagonal can be used to assess the effect of increasing mesh size, and the  
495 opposite diagonal to compare the effect of uneven sieve-panel inclination.

496

497 Figure 3. Sieving efficiency curves (solid lines), bootstrap CIs (dashed lines), and experimental  
498 sieving data (points) obtained by each design (D1= Design 1 ,..., D4= Design 4) on cod (top  
499 rows) and blue whiting (bottom rows). Total catches (light grey shading) and catches in the lower  
500 codend (dark grey shading) are plotted in the background.

501

502 Figure 4. Sieving efficiency curves (solid lines), bootstrap CIs (dashed lines), and experimental  
503 sieving data (points) obtained by each design (D1= Design 1 ,..., D4= Design 4) on American  
504 plaice (top rows) and witch flounder (bottom rows). Total catches (light grey shading) and

505 catches in the lower codend (dark grey shading) are plotted in the background.

506

507 **Supporting material:**

508

509 Figure S1. Map of the fishing area (Skagerrak; ICES Division IIIa), where the experimental sea  
510 trials took place. The top-right panel shows the towing tracks.

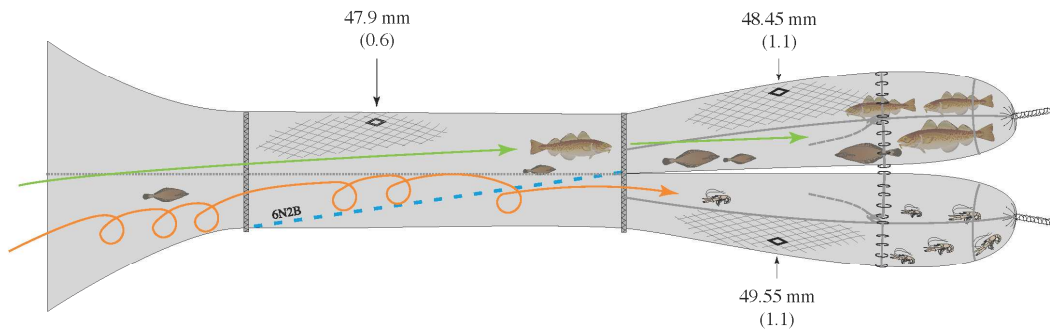
511

512 Figure S2. Pictures taken in shallow waters from Design 1 before beginning experimental  
513 fishing. Above: View of the panel in the middle section with the camera oriented backwards  
514 towards the codends. Below: Insertion of the sieve-panel to the floor of the extension.

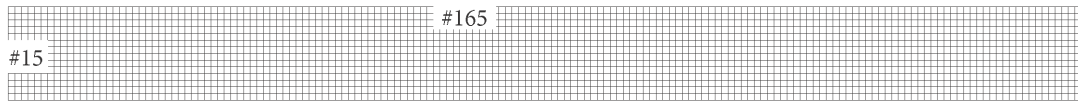
515

516 Figure S3. Left: Screenshots from underwater video recordings taken in haul 25 (Design 3),  
517 showing *Nephrops* individuals actively passing through the sieve-panel. Right: Different  
518 behavioral patterns observed for *Nephrops* on the panel. Arrows point to chelipeds hanging on to  
519 the mesh twines.

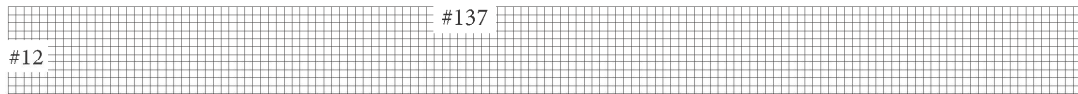
Figure 1



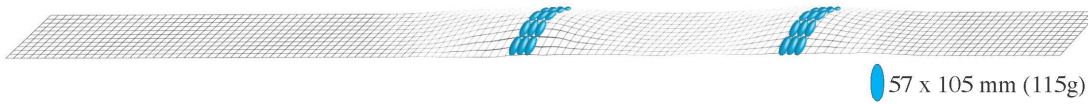
Design 1



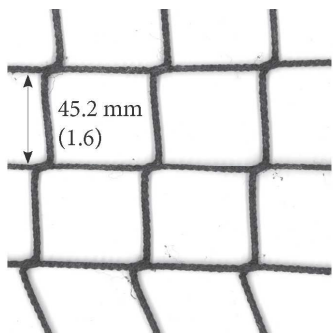
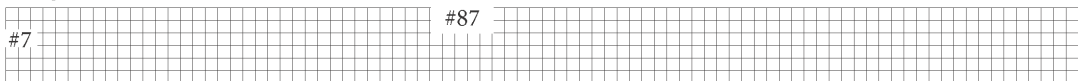
Design 2



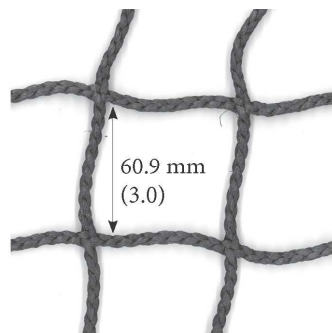
Design 3



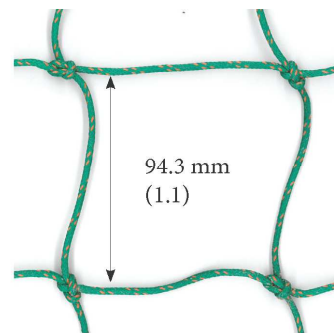
Design 4



Design 1



Design 2 and 3



Design 4

Figure 2

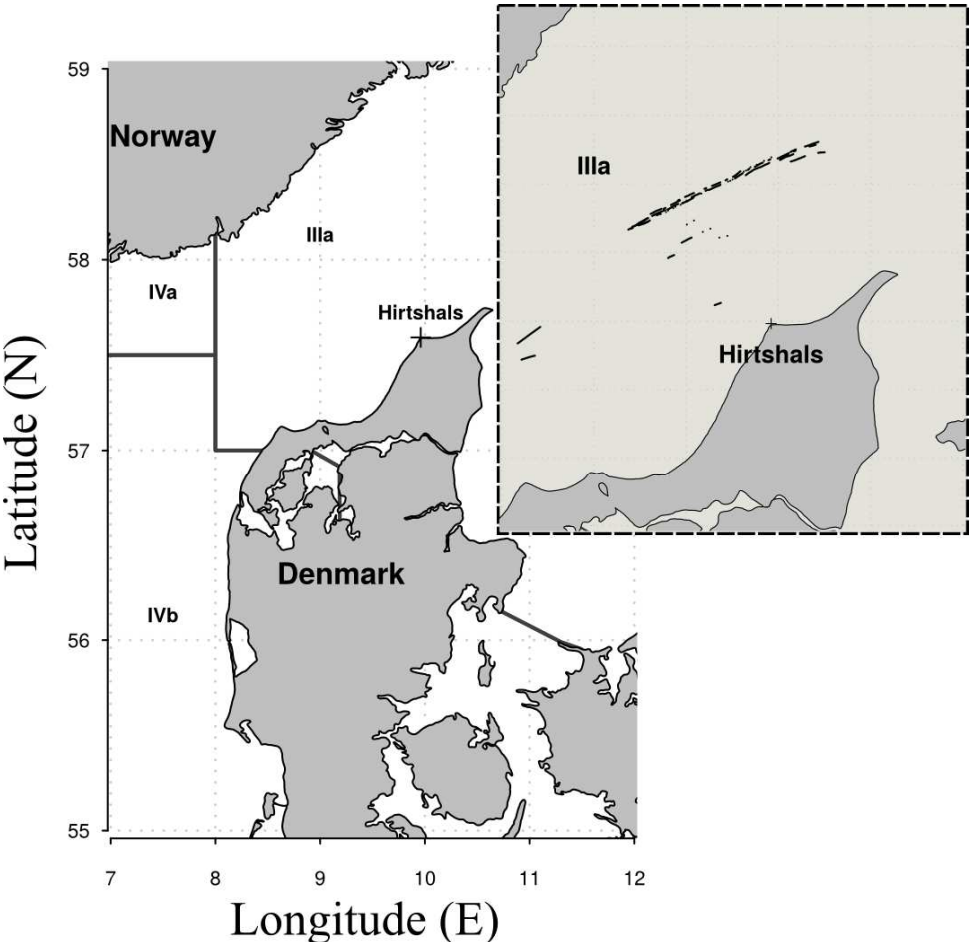


Figure 3

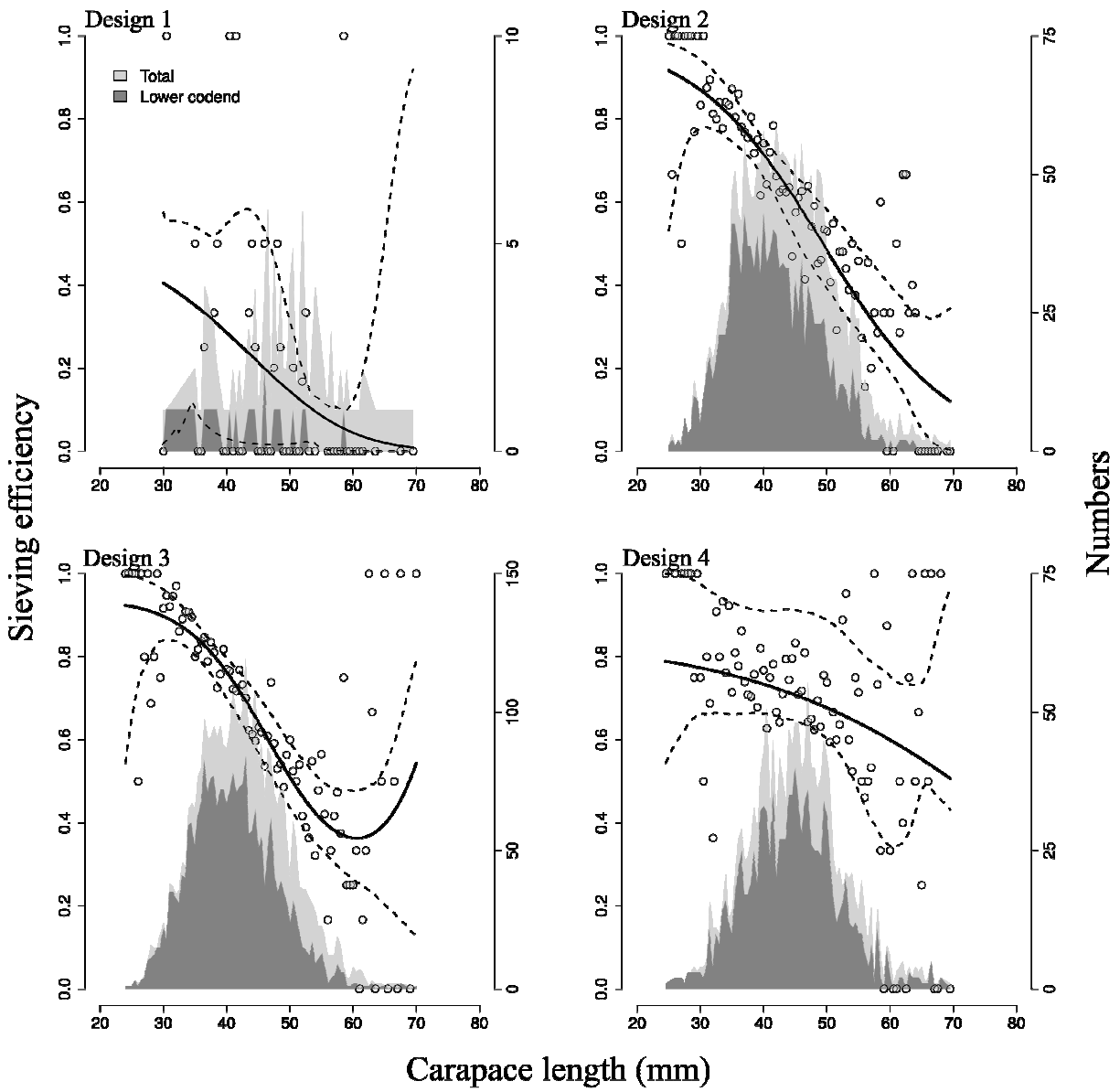


Figure 4

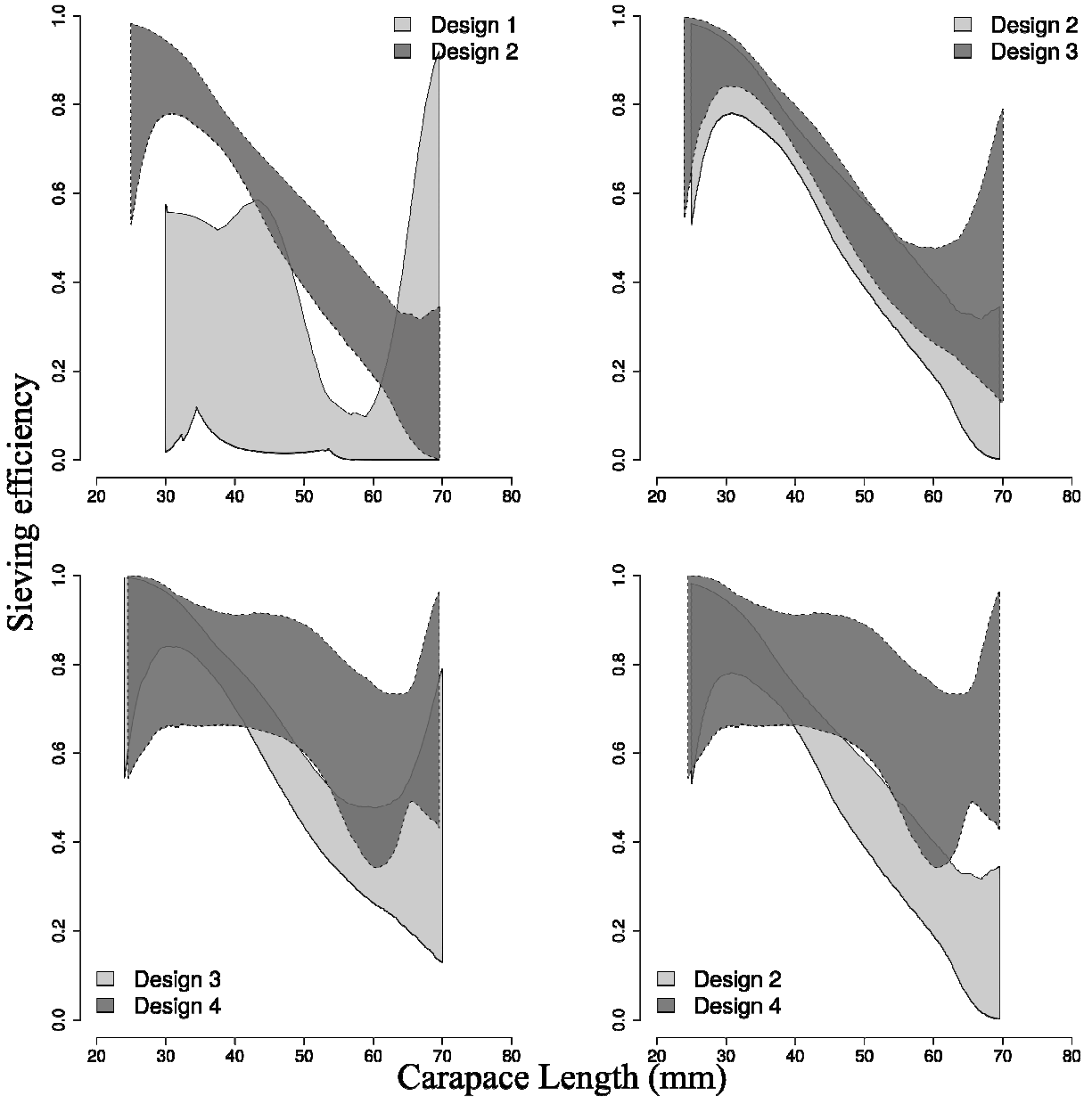


Figure 5

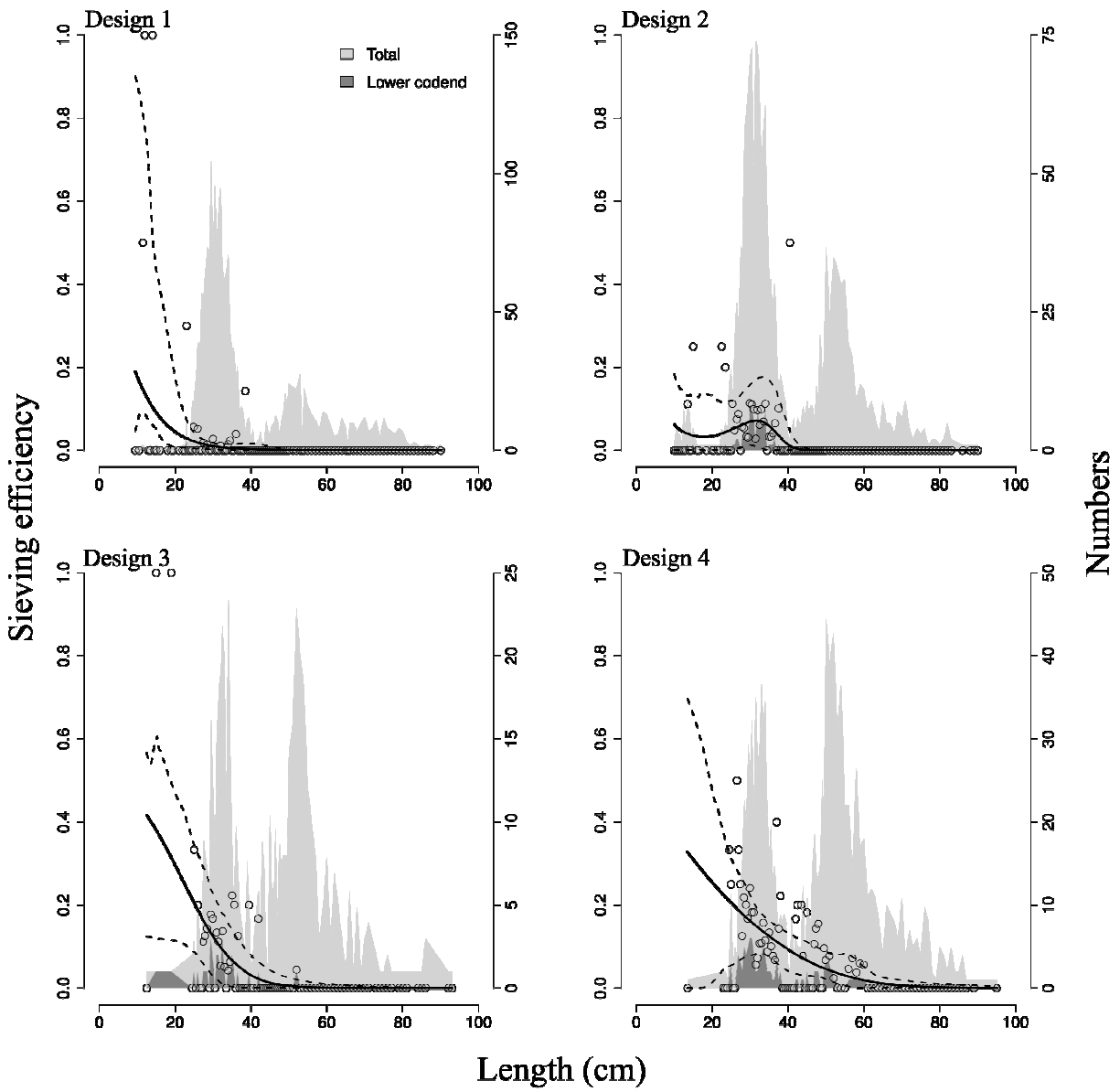




Figure 6

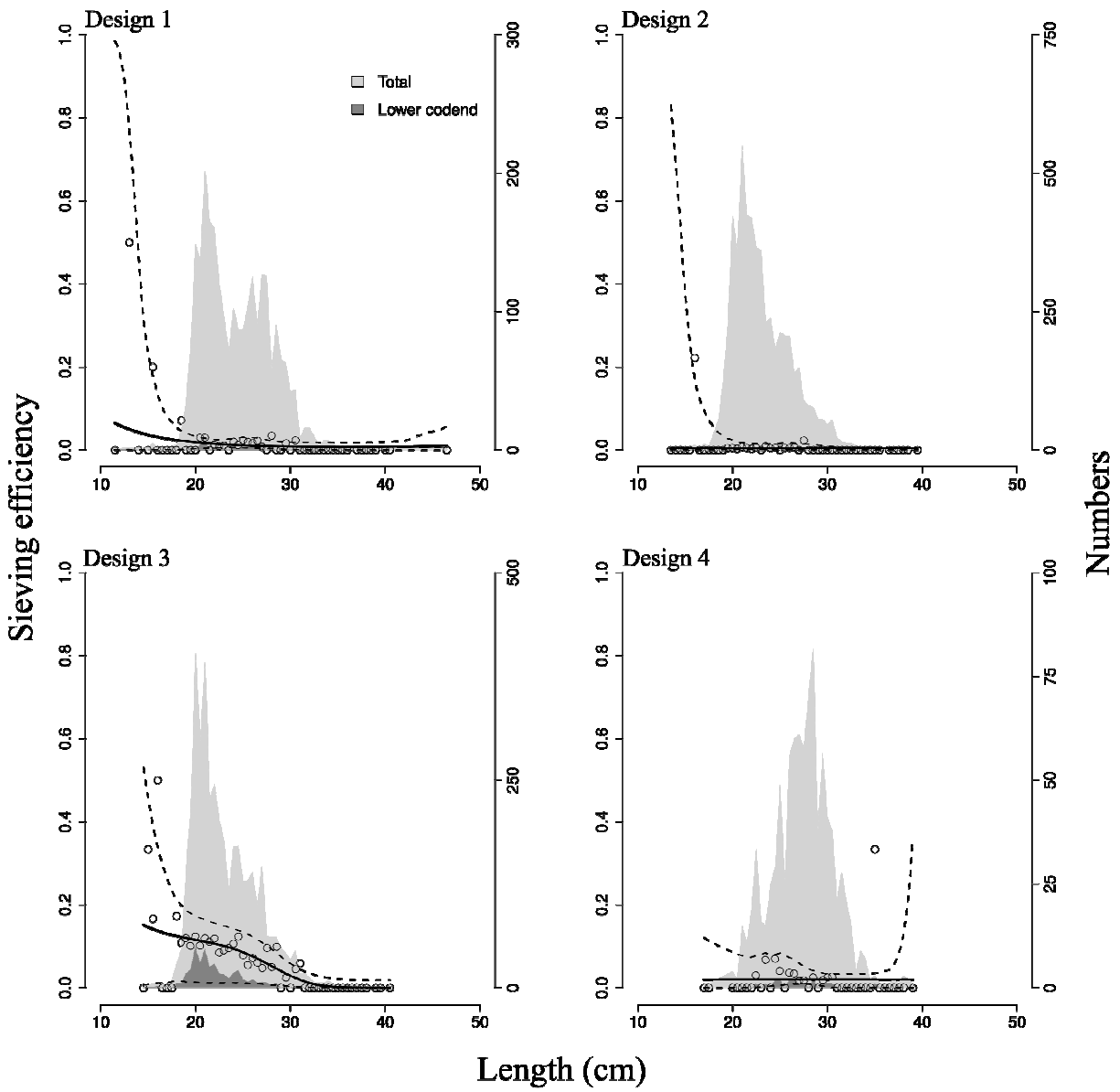


Figure 7

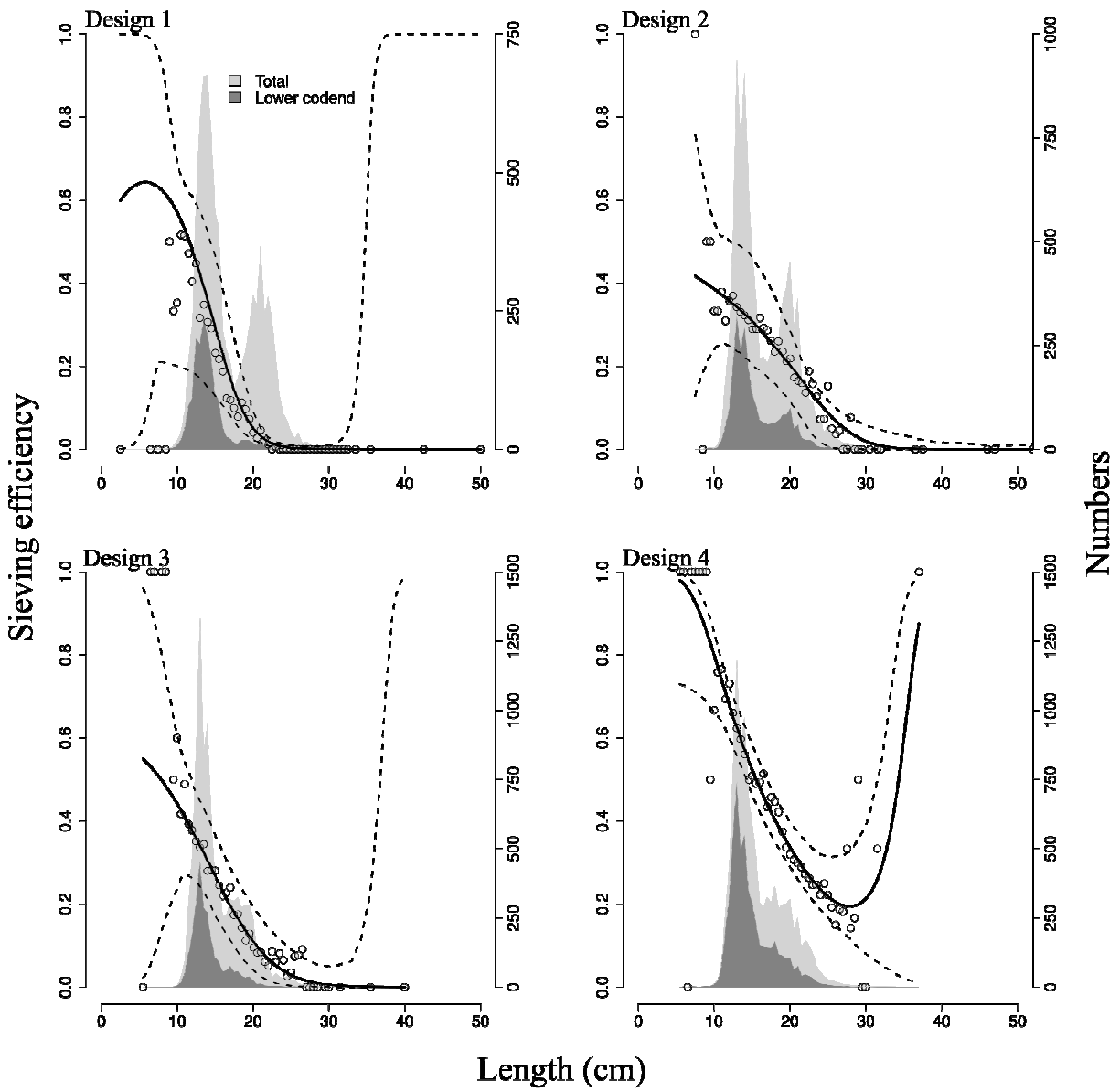


Figure 8

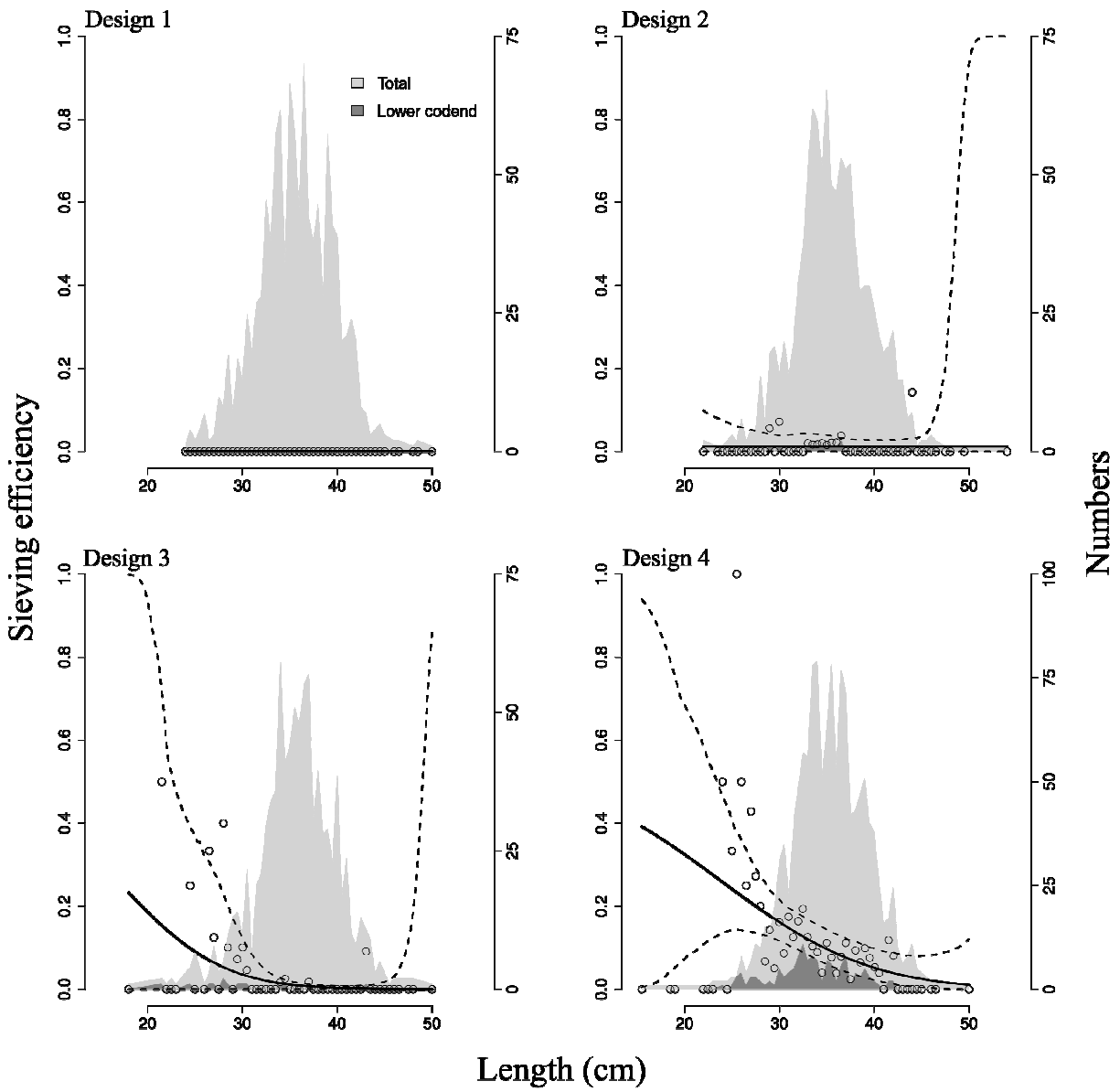


Figure 9

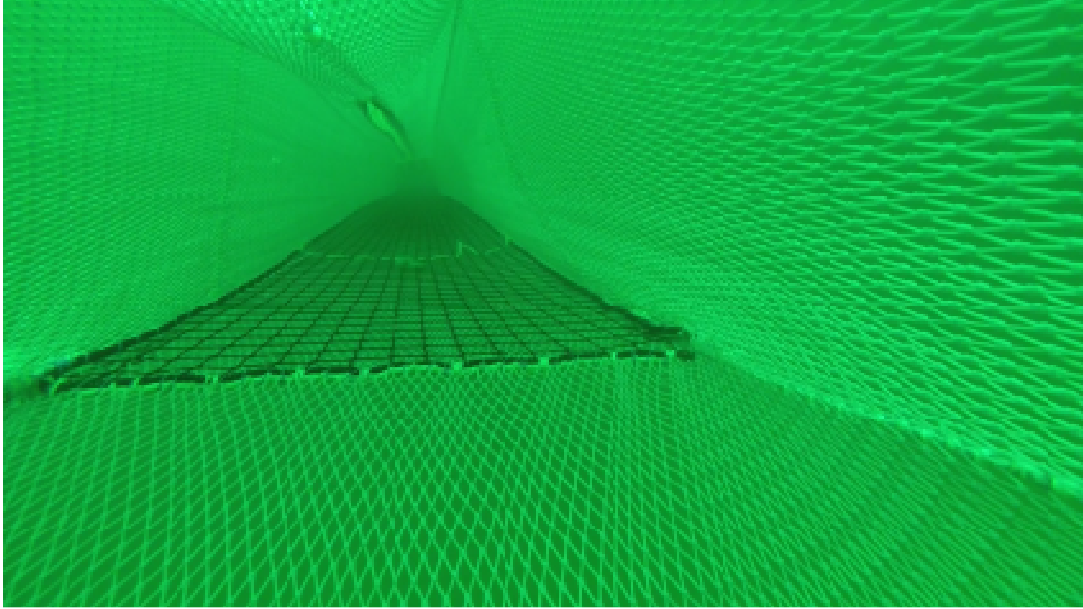
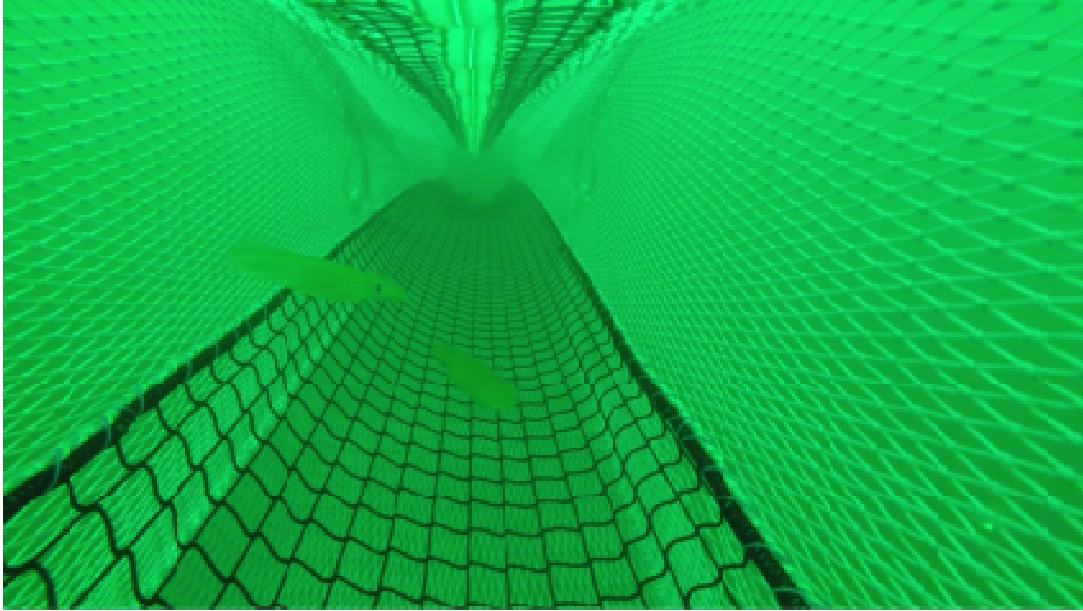


Figure 10

